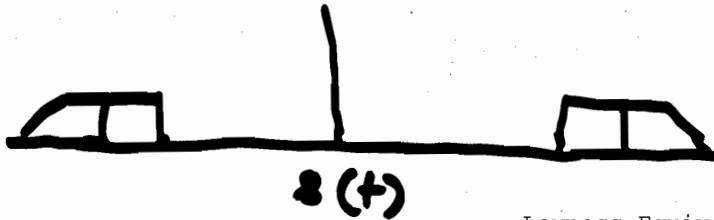


Band Pass Signal Representation

BandPass Signal Representation



Lowpass Equivalent

Low Pass Equivalent

Reasons to modulate

Reasons to modulate

- * Antenna dimension
- * Channel Characteristics
- * Multiplexing
- * Receiver Processing
- * Equipment Cost-



$s(t)$ B.P. Signal
 $s_L(t)$ L.P. Eq. Sig
 $s_+(t)$ Pre Envelope of $s(t)$
 Pre envelope of $s(t)$

B.P. Complex

to keep same energy

$$S_+(f) = 2 U(f) S(f)$$

$$s_+(t) = \int_{-\infty}^{\infty} S_+(f) e^{-j2\pi ft} df$$

\therefore IFT of $S(f)$

$$s_+(t) = \mathcal{F}^{-1}[2U(f)] * \mathcal{F}^{-1}[S(f)]$$

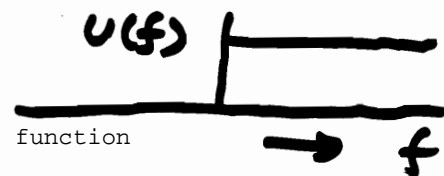
$$s_+(t) = \mathcal{F}^{-1}[2U(f)] * s(t)$$

$$\begin{aligned}
 s_+(t) &= \left(\delta(t) + \frac{j}{\pi t} \right) * s(t) \\
 &= s(t) + \frac{j}{\pi t} * s(t) \\
 &= s(t) + \hat{s}(t)
 \end{aligned}$$



Unit Step $U(f)$

Unit step function



IFT of $2U(f)$

IFT of $2U(f)$

$$\mathcal{F}^{-1}[2U(f)] = \delta(t) + \frac{j}{\pi t}$$

Hilbert-Transform

$$\frac{1}{\pi t} * s(t) = \hat{s}(t)$$

$$\hat{s}(t) = \frac{1}{\pi} \int_{-\infty}^{\infty} \frac{s(\tau)}{t-\tau} d\tau$$



Hilbert Transform

90° phase shifter

$$H(f) = \int_{-\infty}^{\infty} \frac{1}{\pi t} e^{-j\pi ft} dt$$

$$= \begin{cases} -j & ; f > 0 \\ 0 & ; f = 0 \\ +j & ; f < 0 \end{cases}$$

f	↓ ph shift
+ve	-90°
-ve	+90°

Magnitude

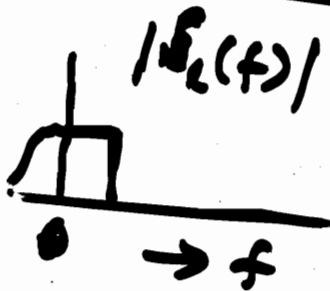
Magnitude

$$|H(f)| = 1 \text{ except } f=0$$

Phase

Phase

$$\angle H(f) = \begin{cases} -\pi/2 & \text{for } f > 0 \\ \pi/2 & \text{for } f < 0 \end{cases}$$



$S_c(t)$ L.P. Eq. of B.P. $\sin 2(t)$

$$S_c(f) = S_+(f + f_c)$$

$$s_c(t) = s_+(t) e^{-j2\pi f_c t}$$

$$\therefore s_c(t) = [s(t) + \hat{s}(t)] e^{j2\pi f_c t}$$

Low Pass Complex Signal (B. Band Signal)

Let $s_c(t)$ has real & imaginary components

$$s_c(t) = x(t) + jy(t)$$

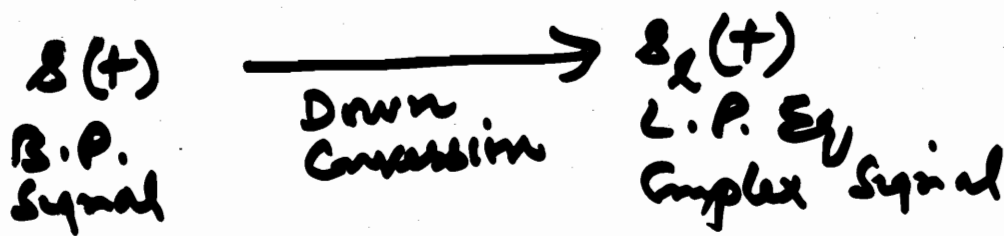
$$[s(t) + j\hat{s}(t)] = [x(t) + jy(t)] e^{j2\pi f_c t}$$

$$x(t) = s(t) \cos(2\pi f_c t) + \hat{s}(t) \sin(2\pi f_c t)$$

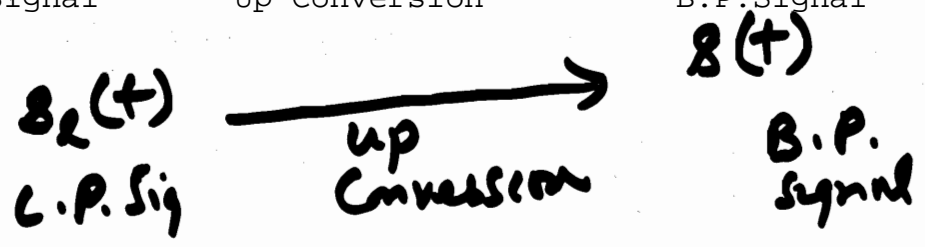
$$y(t) = -s(t) \sin(2\pi f_c t) + \hat{s}(t) \cos(2\pi f_c t)$$

but $s_+(t) = s(t) + \hat{s}(t)$
but $s_+(t) = s(t) + s^*(t)$

$$j\hat{s}(t) = (-j \sin 2\pi f_c t)$$



B.P. Signal-----Down Conversion-----L.P. Eq. Complex Signal
 L.P. Signal-----Up Conversion-----B.P. Signal



L.P. to B.P.

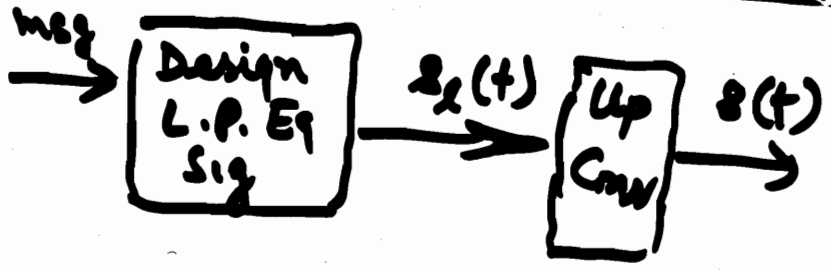
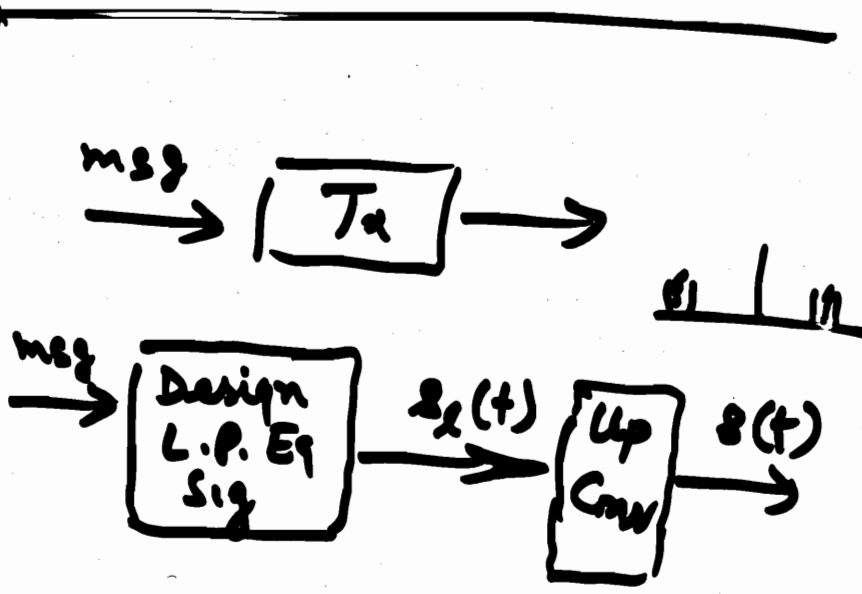
L.P. to
B.P.

$$s_c(t) = x(t) + jy(t)$$

$$s(t) = x(t) \cos 2\pi f_c t - y(t) \sin 2\pi f_c t$$

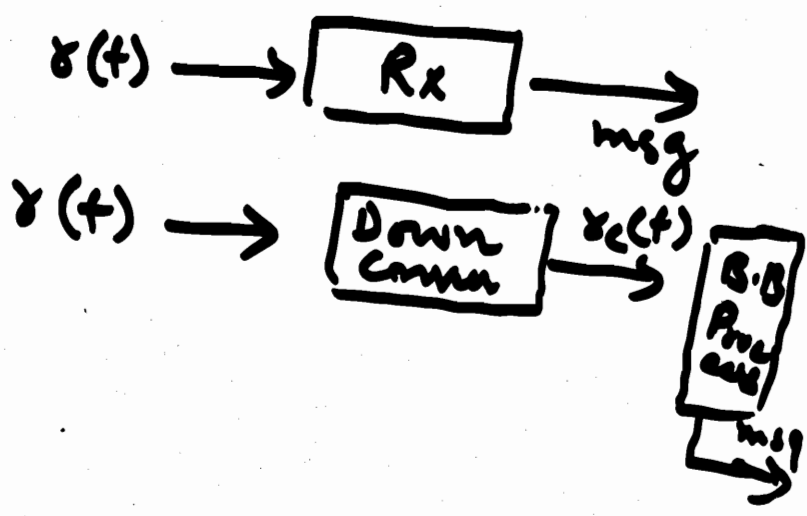
$$\hat{s}(t) = x(t) \sin 2\pi f_c t + y(t) \cos 2\pi f_c t$$

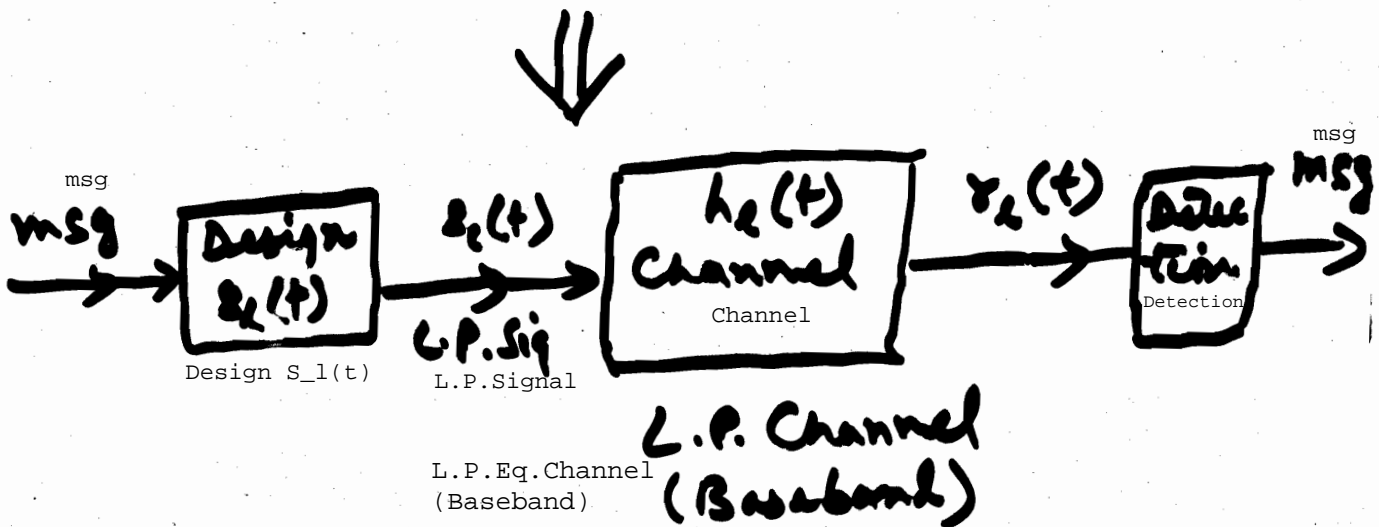
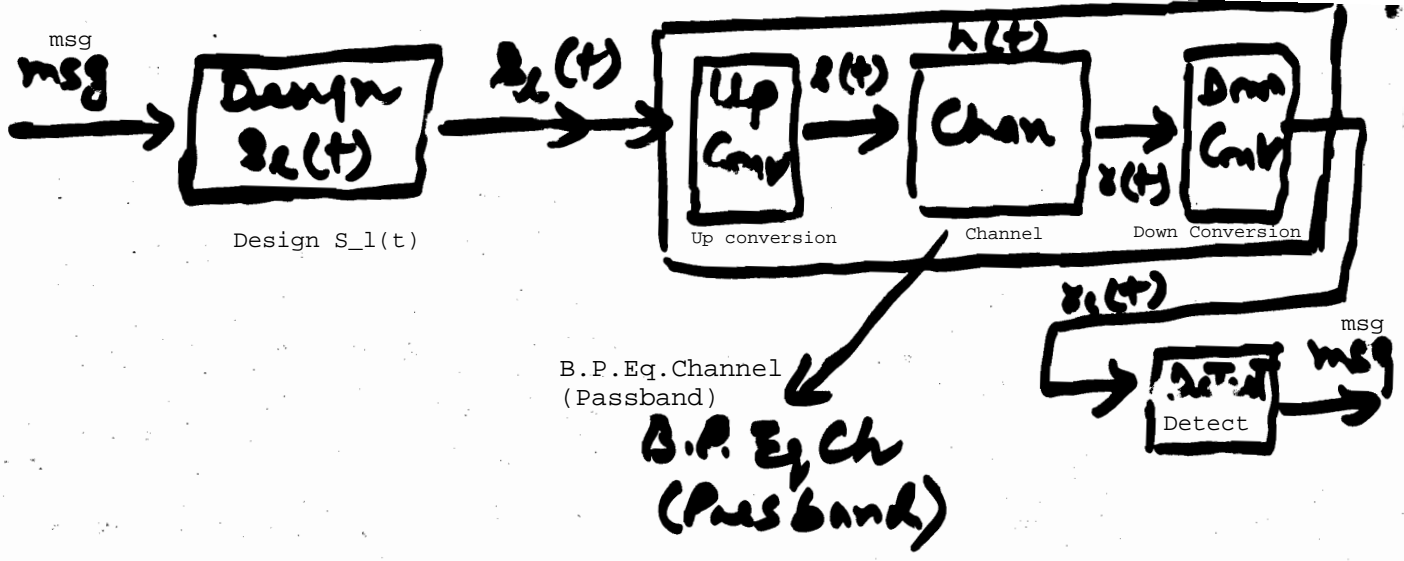
$\therefore s_c(t) = s(t) + j\hat{s}(t)$
 $\therefore S_c(f) = \frac{S(f) e^{-j2\pi f_c t}}{[S(f) + j\hat{S}(f)]}$



$\therefore s(t)$ processing complex costly in H.F.
 So bring down to L.P. Eq & process in B. Band

$r(t)$ processing complex Costly in H.F.
 so bring down to L.P. Eq. & Process in B. Band

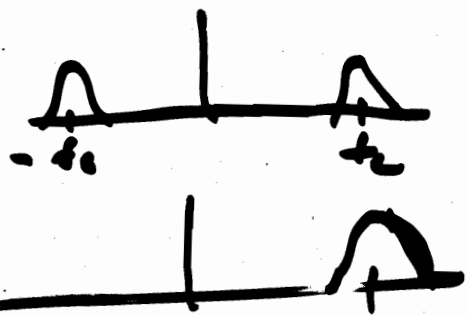




L.P. Channel (Baseband)

Complex Channel Complex Signal

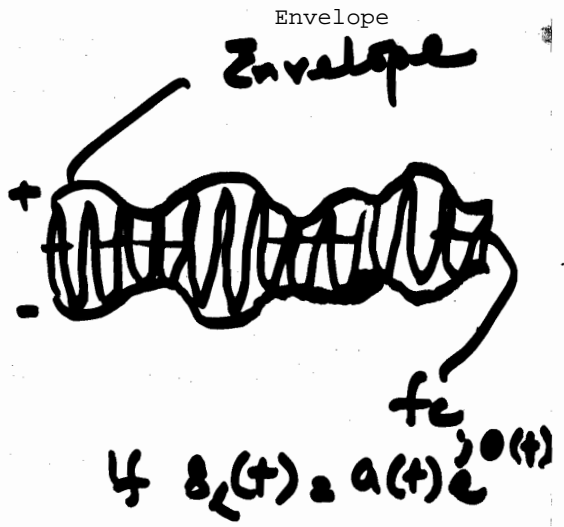
Envelope



B.P. Signal

Suppress by Unit Impulse to get one sided signal

Suppress by Unit Impulse to get one sided sig



$$s_c(t) = a(t) e^{j2\pi f_c t}$$

Shift the spectrum to get L.P. Eq. Sig

Shift the spectrum to get L.P. Eq.

$$a(t) = \sqrt{x^2(t) + y^2(t)}$$

$$\theta(t) = \tan^{-1} \left(\frac{y(t)}{x(t)} \right)$$

Envelope Phase

$$s_c(t) = \text{Re} [a(t) e^{j2\pi f_c t + j\theta(t)}]$$

$$s_c(t) = a(t) \cos(2\pi f_c t + \theta(t))$$

Energy of a B.P. Signal

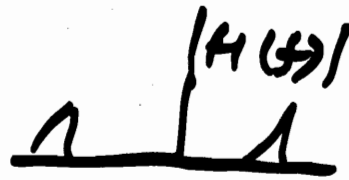
$$E = \int_{-\infty}^{\infty} s^2(t) dt \approx k_2 \int_{-\infty}^{\infty} |s_c(t)|^2 dt$$

I.R. of a B.P. System $H(f)$

I.R. of a B.P. System $H(f)$

real, bandpass

$h(t) \rightarrow$ real, bandpass



$$H(f) = H^*(-f)$$

conjugate Shift

Conjugate Shift

$$H_+(f) = \begin{cases} H(f) & \forall f > 0 \\ 0 & \forall f < 0 \end{cases}$$



~~$H_+(f) = H_+(f)$~~ $H_+(f) = U(f)H(f)$

$$H_c(f) = H_c(f + f_c)$$

$$H_c(f - f_c) = \begin{cases} H(f) & ; f > 0 \\ 0 & ; f < 0 \end{cases}$$

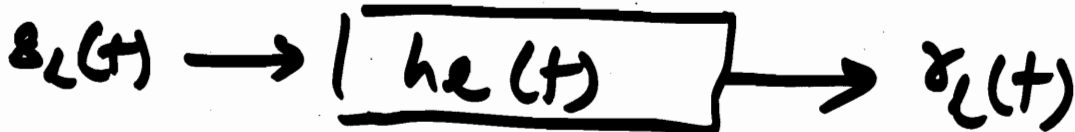
$$H(f) = H_c(f - f_c) + H_c^*(-f - f_c)$$

$$\begin{aligned} h(t) &= h_c(t) e^{j2\pi f_c t} + h_c^* e^{-j2\pi f_c t} \\ &= 2 \operatorname{Re} [h_c(t) e^{j2\pi f_c t}] \end{aligned}$$



\downarrow LPF
LPEq

\downarrow LPF
LPEq



$$s(t) = \text{Re} [s_1(t) e^{j2\pi f_c t}]$$

CG-5

$$s(t) = \text{Re} [s_2(t) e^{-j2\pi f_c t}]$$

$$h(t) = 2\text{Re} [h_2(t) e^{j2\pi f_c t}]$$

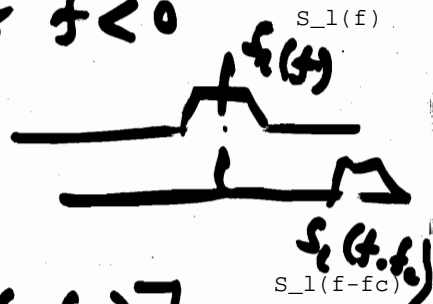
$$R(f) = S(f) H(f)$$

$$= \frac{1}{2} [S_2(f-f_c) + S_2^*(-f-f_c)]$$

$$= [H_2(f-f_c) + H_2^*(-f-f_c)]$$

$s_2(t), h_2(t) \rightarrow$ narrowband signals

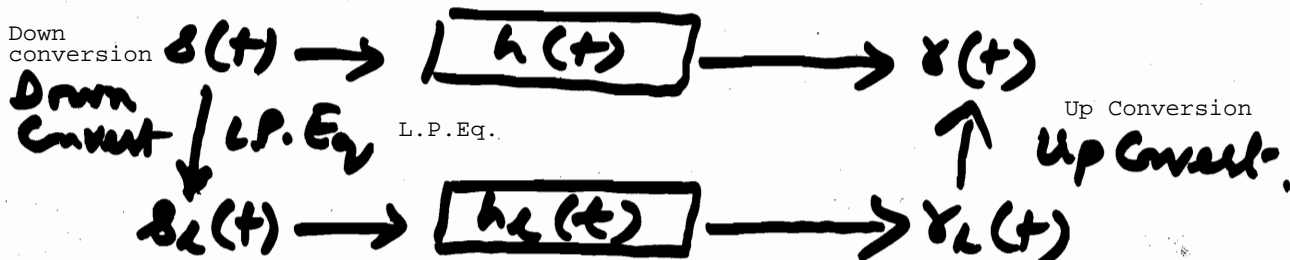
So $S_2(f-f_c) = 0$ for $f < 0$

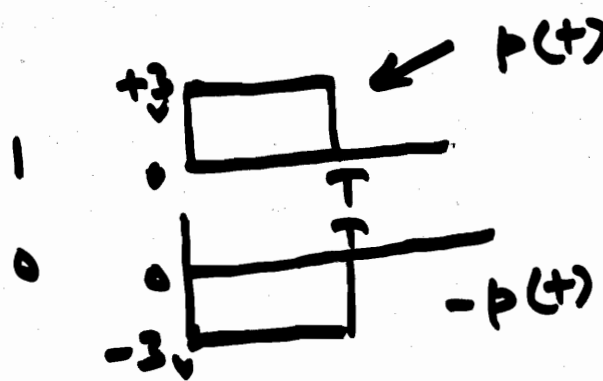


$$R(f) = \frac{1}{2} \left[S_2(f-f_c) H_2(f-f_c) + S_2^*(-f-f_c) H_2^*(-f-f_c) \right]$$

$$R(f) = \frac{1}{2} [R_2(f-f_c) + R_2^*(-f-f_c)]$$

$$R_2(f) = S_2(f) H_2(f)$$





Mapping
 1 → +3V
 0 → -3V

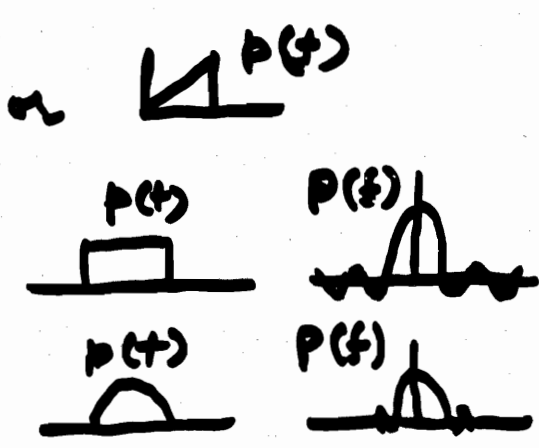
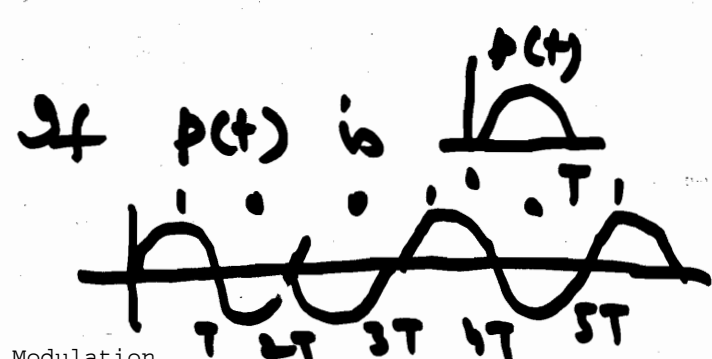
1 0 0 1 0 1



1 1 0 0 1 0 1
 . . . b₁ b₂ b₃
 a₁ a₂ a₃

a₀ p(t)
 a₁ p(t-T)
 a₂ p(t-2T)

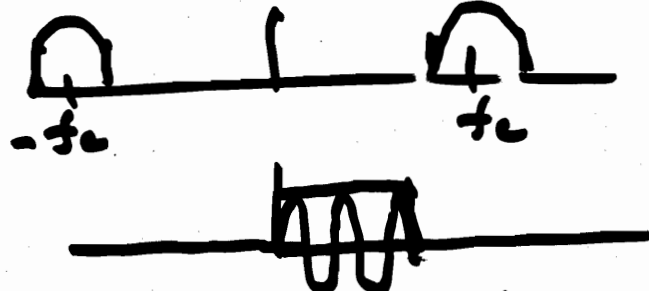
$$x(t) = \sum_{k=0}^{\infty} a_k p(t-kT)$$



Passband Modulation

Passband Modulation

If p(t) is passband



$$p'(t) = p(t) \sin(2\pi f_c t)$$

$$= \frac{1}{2j} p(t) (e^{j2\pi f_c t} - e^{-j2\pi f_c t})$$

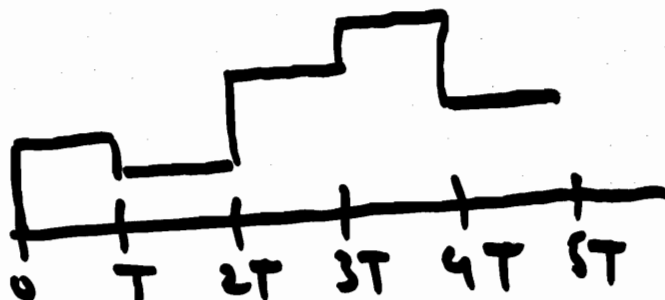
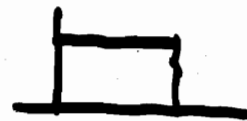
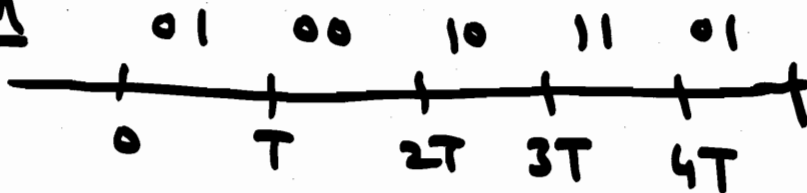
$$= \sum_{k=0}^{\infty} a_k p'(t-kT)$$

$$b(t) = \sum_{k=0}^{\infty} a_k p(t-kT)$$



Q-PAM

CG-8



Advantage: More bits/s

Ad: - more bit/s

disadvantage: More Power

disAd: - more power

Avg power

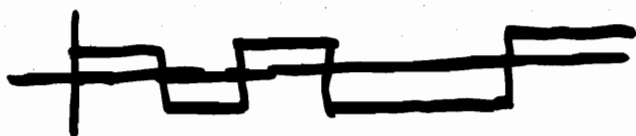
If we increase the levels the noise probability increases

If we increase the levels the noise probability increases

M-PAM

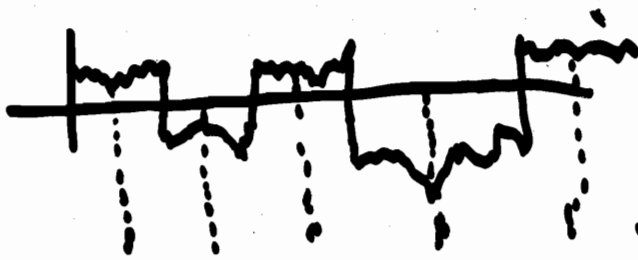
$$M = 2^b$$

$$b \text{ bits} = 2^b \text{ levels}$$



AWGN (-inf --- inf)

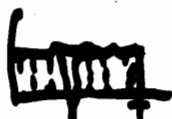
AWGN (- ∞ - ∞)
Noise effect



Noise Effect

sampling instant

Sampling Instant



error

Integrate to demodulate

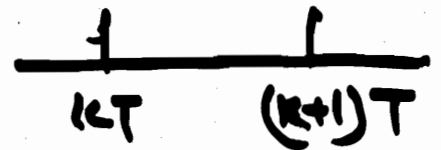
integrate to demodulate

$$\int_0^T y(t) dt$$

Demodulation

$$x(t) \rightarrow a_k \rightarrow b_k$$

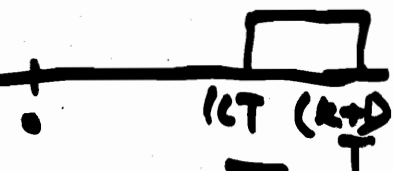
$$\hat{a}_k = \int_{kT}^{(k+1)T} x(t) dt$$



$$= \int_{-\infty}^{\infty} x(t) p(t - kT) dt$$



$$= \int_{-\infty}^{\infty} x(t) p(T - (k+1)T + t) dt$$



$$p(T-t) * x(t) \Big|_{t = \frac{(k+1)T}{2}}$$

\downarrow
 $y(t)$

$$\int y((k+1)T - t) x(t) dt$$

